

# Cocrystallization of poly(vinylidene fluoride) and vinylidene fluoride–tetrafluoroethylene copolymers:

## 2. Thermodynamic study

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The phase diagrams of poly(vinylidene fluoride) (PVF<sub>2</sub>; KF and KY) and vinylidene fluoride–tetrafluoroethylene (VF<sub>2</sub>–VF<sub>4</sub>) copolymers (Cop-1, Cop-2) have been reported. They are the KF/KY, Cop-1/Cop-2, KF/Cop-1 and KY/Cop-1 systems. The head to head (H–H) defect structures of KF, KY, Cop-1 and Cop-2 are 3.5, 5.3, 15.8 and 21.3 mol%, respectively. The KF/KY and Cop-1/Cop-2 blends exhibit linear variation of apparent melting points with composition but the KF/Cop-1 and KY/Cop-1 blends show a bifurcation of melting point–composition diagram at the Cop-1 rich regions. The crystallization temperature ( $T_c$ )–composition plots are linear except for the KF/Cop-1 system. The anomaly of the KY/Cop-1 system in this regard has been explained. The equilibrium melting points ( $T_m^0$ ) of the blends were determined using the Hoffman–Weeks procedure. The KF/KY blends show a slightly concave upward  $T_m^0$  vs. composition curve indicating weak interaction of the components. The Cop-1/Cop-2 blends exhibit a linear plot over the same composition due to ideal mixing. Both the KF/Cop-1 and KY/Cop-1 blends exhibit a concave upward curve with some concave downward portion for the  $T_m^0$  vs. composition plots at the Cop-1 rich regions. Further, at the Cop-1 rich regions ( $W_{\text{Cop-1}} = 0.75$ ), three melting peaks of isothermally crystallized KF/Cop-1 and KY/Cop-1 blends were observed when melted from the  $T_c$ s. Liquid–liquid phase separation in the melt for the KF/Cop-1 and KY/Cop-1 systems at Cop-1 rich compositions has been attributed to the different behaviour rather than observed from the other pairs. The cocrystallization of this system is complicated by both the crystalline phase segregation and the liquid–liquid phase segregation. Copyright © 1996 Elsevier Science Ltd.

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### INTRODUCTION

Recently, crystalline polymer blends have been intensively investigated from the viewpoint of cocrystallization. They are the blends of polyethylene of different commercial grades<sup>1–5</sup>, poly(vinyl fluoride) and poly(vinylidene fluoride)<sup>6,7</sup>, vinylidene fluoride–trifluoroethylene (VF<sub>2</sub>–VF<sub>3</sub>) copolymers<sup>8</sup>, poly(tetrafluoroethylene) and poly(tetrafluoroethylene-co-perfluoroalkyl-vinyl ether)<sup>9</sup>, etc. However, there is a lack of complete thermodynamic studies in most of these systems. In this paper we present a thermodynamic study of such a system using poly(vinylidene fluoride) (PVF<sub>2</sub>) and vinylidene fluoride–tetrafluoroethylene (VF<sub>2</sub>–VF<sub>4</sub>) copolymers.

Both PVF<sub>2</sub> and VF<sub>2</sub>–VF<sub>4</sub> copolymers contain different amounts of head to head (H–H)/pseudo head to head defect structure in their chain<sup>10,11</sup>. Earlier we had established the cocrystallization possibilities among the different defect content samples and also reported the influence of crystallization temperature on the cocrystallization of the above polymers at the 1/1 composition of the mixture<sup>12</sup>. It was established from these studies

that cocrystallization of PVF<sub>2</sub> and VF<sub>2</sub>–VF<sub>4</sub> copolymer is limited to the difference of 12 mol% H–H defect structure in the chains of the two components. In order to understand the cocrystallization process of these polymers more explicitly we studied the phase diagrams of the mixtures and determined the results presented here.

The phase diagrams (melting point–composition plots) of binary mixtures of crystalline polymers (miscible in melt) are generally of four different types<sup>8</sup>: (a) immiscible with eutectic; (b) immiscible with no eutectic; (c) miscible with concave upward (weak interaction); and (d) miscible with concave downward (strong interaction). Tanaka *et al.* studied the phase diagrams of the blends of vinylidene fluoride–trifluoroethylene (VF<sub>2</sub>–VF<sub>3</sub>) copolymers and observed that they belonged to type II and type III classes depending upon the difference of co-unit concentration of the components<sup>8</sup>. Keller and his co-workers made extensive studies of the phase diagrams of linear polyethylene (LPE) with branched polyethylene (BPE) and observed that they did not produce cocrystals at all compositions<sup>4,13,14</sup>. From both the d.s.c. and morphology studies they concluded that the blends of BPE rich regions are biphasic in nature and

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attributed it to the liquid-liquid phase separation of the melt at this composition. However, in a recent paper, Alamo *et al.* reported from small angle neutron scattering studies that there is no liquid-liquid phase separation in this system and the biphasic nature of the blend is due to the crystallization process<sup>15</sup>. These contradictory reports on the cocrystallization mechanism of this system needs to be studied in other systems. PVF<sub>2</sub> and VF<sub>2</sub>-VF<sub>4</sub> copolymers are an ideal pair in this regard and a thermodynamic study may help to delineate the mechanism of cocrystallization in this system.

## EXPERIMENTAL

The characteristics of the samples used in the work are presented in Table 1<sup>12</sup>. Pairs of these polymers were mixed in different composition by dissolving in *N,N*-dimethyl formamide at 80°C followed by evaporation of the solvent at 60°C. They were finally dried at 70°C for 3 days. Here it is necessary to mention that the KF and KY PVF<sub>2</sub> crystallizes in the  $\alpha$  phase whereas the Cop-1 and Cop-2 crystallize in the  $\beta$  phase when crystallized from the melt<sup>12</sup>.

In the thermodynamic study we choose the experiments in three different directions: (a) measurement of the apparent melting points of the blends crystallized at different temperatures; (b) measurement of the crystallization temperatures ( $T_c$ ) of the blends crystallized from the melt at a cooling rate of 2.5° min<sup>-1</sup>; and (c) measurement of the equilibrium melting points of the blends. In the first set of experiments the apparent melting points of the whole composition of the blends are reported from crystallization at three different crystallization temperatures, e.g. (a) at 50°C, (b) at 120°C and (c) at 135°C. For crystallization at 50°C about 5 mg of the samples were used and melted at 227°C in the d.s.c. for 10 min. They were then quenched at 200°C min<sup>-1</sup> to 50°C and kept for 10 min before starting the melting run. The crystallization at 120°C and 135°C were carried out by sealing the d.s.c. capsules in glass tubes under vacuum (10<sup>-4</sup> torr). They were melted in a thermostatic bath set at 227°C for 10 min and quickly transferred to another bath set at the predetermined crystallization temperature. Sufficient time for crystallization was given in each case and in each series of blends the same time of crystallization has been given so that comparison can be done fruitfully. KF and KY PVF<sub>2</sub> samples exhibit melt recrystallization<sup>16,17</sup> and to eliminate the melt recrystallization of their blends they were crystallized for five days at both temperatures. The melting of the cocrystals was studied in a Perkin-Elmer DSC-7 equipped with 3700 data station at the heating rate of 10° min<sup>-1</sup>. The instrument was calibrated with indium before use. The peak temperatures were taken as the melting points.

The measurement of crystallization temperatures ( $T_c$ ) were carried out by the dynamic cooling method. The samples were melted at 227°C and cooled at 2.5° min<sup>-1</sup> and the exotherms were recorded. The exothermic peak temperature was taken as  $T_c$ s.

For the measurement of equilibrium melting points isothermal crystallizations were performed by melting the samples at 227°C and then rapidly quenched to the predetermined isothermal crystallization temperature. After crystallization for different times they were heated from this temperature at 10° min<sup>-1</sup> without cooling. The peak melting temperatures were plotted against crystallinity and the melting points at 10% crystallinity was taken as a measure of  $T_m$  at each  $T_c$ . The melting points of the  $\alpha$  and  $\beta$  phases (where it was produced) only were considered here. No melting study on  $\gamma$  and  $\gamma'$  phases was made.

## RESULTS AND DISCUSSION

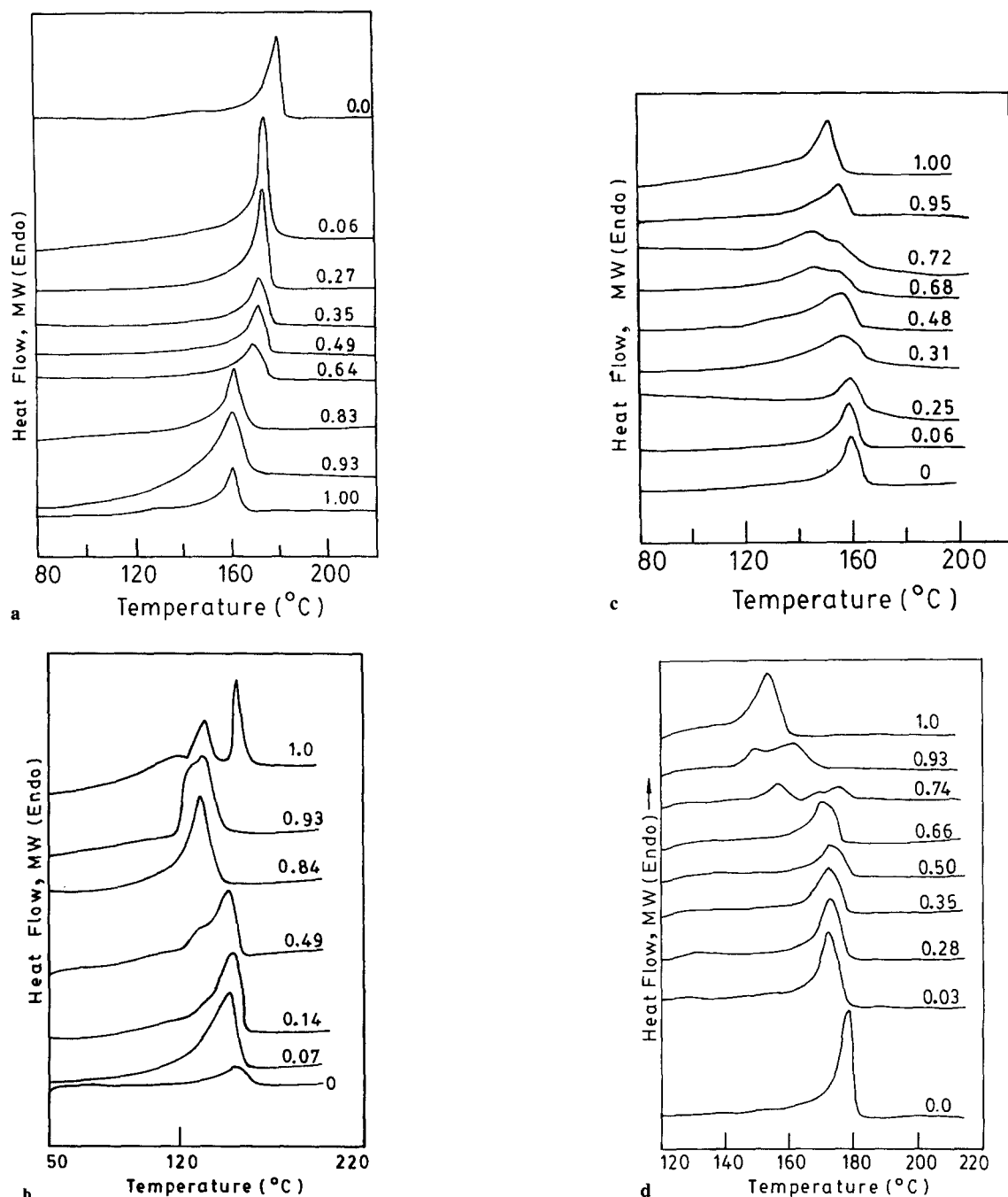
### Apparent melting points

In Figure 1(a-d) the melting endotherms are shown for the samples crystallized at 120°C. In Figure 1a the endothermic peaks are very sharp for all compositions indicating that KF and KY PVF<sub>2</sub> have cocrystallized at this temperature over the whole composition range. The melting endotherms of Cop-1/Cop-2 blends (Figure 1b) are broader than those of the earlier pair but it is apparent from the figure that co-crystallization is taking place for all compositions because the characteristic higher melting peak of Cop-2 is absent in the blends. In Figure 1c the melting endotherms of KY/Cop-1 blends are presented. From the figure it is clear that the endothermic peaks are broader with increasing Cop-1 content and at  $W_{\text{Cop-1}} = 0.68$  and 0.72 the two peaks of the components are clearly resolved indicating no cocrystallization at these compositions. However, at  $W_{\text{Cop-1}} = 0.95$  no multiplicity of the melting peak is found indicating complete co-crystallization at this composition. In Figure 1d melting endotherms of the KF/Cop-1 system are presented. Here also, with increasing Cop-1 concentration in the blend, the peaks became broader and at  $W_{\text{Cop-1}} = 0.74$  and 0.93 multiplicity in the melting peaks was observed. Thus at these two compositions co-crystallization does not take place. From these results it is apparent that if the difference of H-H defect concentration of the components increases cocrystallization is less favoured and with increasing concentration of the higher H-H defect component in the blend the situation also becomes worse.

To understand the effect of crystallization temperature on the cocrystallization process we studied the systems by crystallizing at two other temperatures. In Figures 2a and b typical melting endotherms of KF/Cop-1 blends

**Table 1** Characteristics of the PVF<sub>2</sub> and (VF<sub>2</sub>-VF<sub>4</sub>) copolymer samples

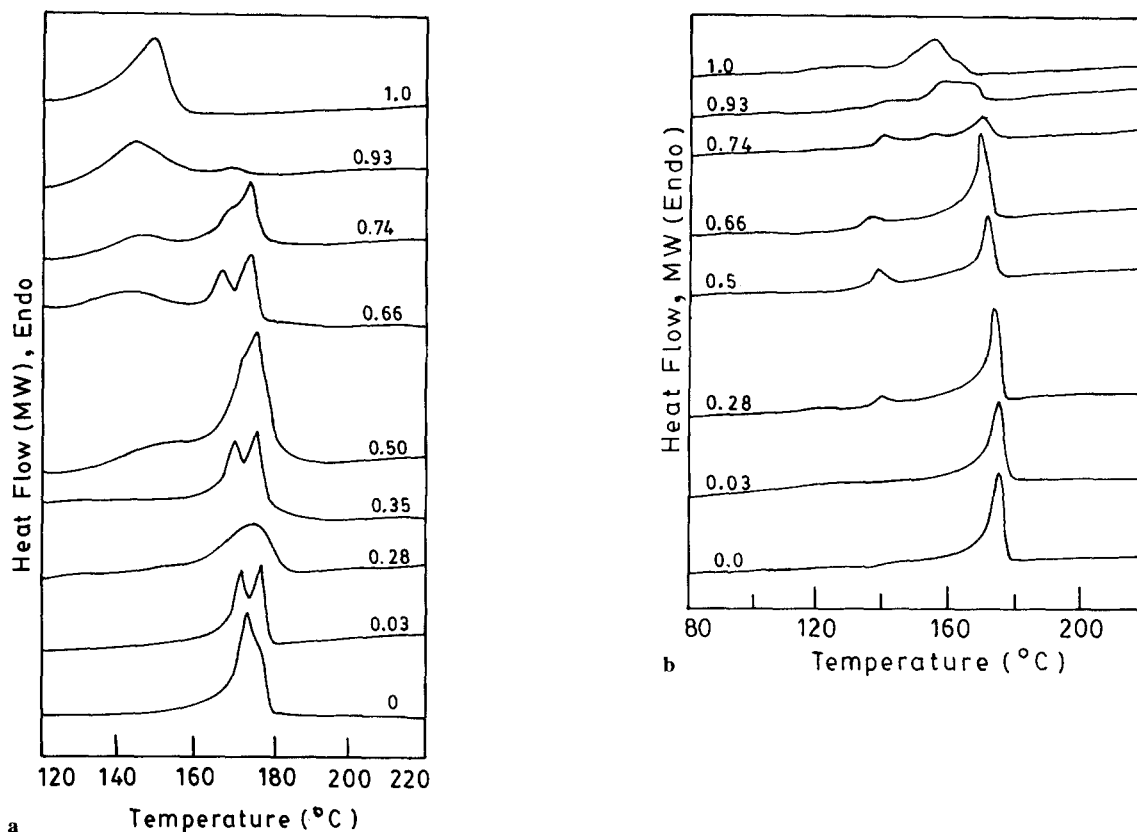
Sample	$\bar{M}_w \times 10^{-5}$	PDI	VF <sub>4</sub> content (mol%)	H-H defect (mol%)	Polymorph
KF	4.28	1.47	0.00	3.5	$\alpha$
KY	7.36	2.04	0.00	5.31	$\alpha$
Cop-1	1.97	2.07	9.1	15.8	$\beta$
Cop-2	3.23	2.63	14.3	21.3	$\beta$



**Figure 1** (a) Melting endotherms of KF/KY blends crystallized at 120°C for 5 days at the indicated weight fractions of KY PVF<sub>2</sub>. (b) Melting endotherms of Cop-1/Cop-2 blends crystallized at 120°C for one day at the indicated weight fractions of Cop-2. (c) Melting endotherms of KY/Cop-1 blends crystallized at 120°C for five days at the indicated weight fractions of Cop-1. (d) Melting endotherms of KF/Cop-1 blends crystallized at 120°C for five days at the indicated weight fraction of Cop-1

are presented for samples crystallized at 50°C and 135°C respectively. In *Figure 2a* the melting endotherms of KF/Cop-1 blends crystallized at 50°C are shown. It is apparent from the figure that for the blends of compositions  $W_{\text{Cop-1}} \geq 0.5$  two melting peaks are observed, the lower correspond to the melting of Cop-1 and the higher for that of KF. For compositions  $W_{\text{Cop-1}} < 0.5$  two peaks are observed in some cases, however, none of these correspond to melting of Cop-1 and this indicates that the blends of compositions  $W_{\text{Cop-1}} < 0.5$  are producing cocrystals. The double peaks at compositions  $W_{\text{Cop-1}} < 0.5$ , therefore, arise due to the melt-recrystallization and the melt recrystallization vanishes for crystallization at 120°C (*Figure 1b*)

for five days. In *Figure 2b* the melting endotherms of the samples crystallized at 135°C are shown. From the figure, it is clear that there are multiple melting peaks of blends having compositions  $W_{\text{Cop-1}} \geq 0.28$ . Two melting peaks (at 142°C and at 173°C) are clearly seen in the blends with one intermediate shoulder at ~155°C in some cases. These 142° peaks were absent for crystallization at 50° and also at 120°C. The melting point of Cop-1 (crystallized at 135°C) is 155°C, so the reason for such a low temperature peak at ~142°C may be due to a fraction of the Cop-1 having very high H-H defect concentration. Such a fractionation process during crystallization is quite possible because the temperature 135°C is the isothermal



**Figure 2** (a) Melting endotherms of KF/Cop-1 blends quenched at 50°C at the indicated weight fraction of Cop-1. (b) Melting endotherms of KF/Cop-1 blends crystallized at 135°C for five days at the indicated weight fraction of Cop-1

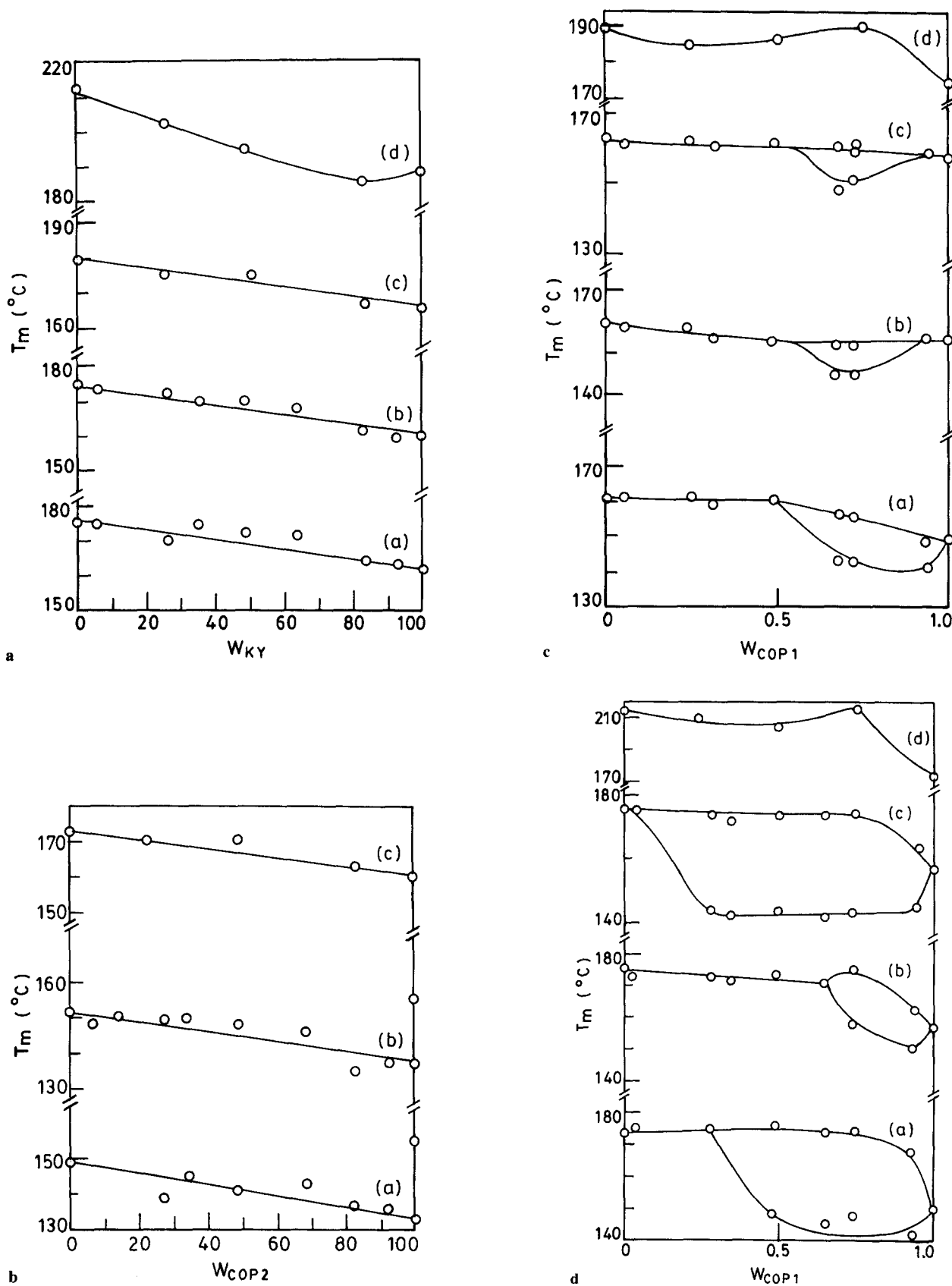
region for crystallization of Cop-1 and the undercooling difference of the two components is very large (40°). The lower defect content fraction of Cop-1 produces co-crystal with KF except the compositions 0.74 and 0.93 where three melting peaks are clearly observed. In the KY/Cop-1 system this type of phase segregation is not favoured because the undercooling difference of the two components is smaller (16°).

To delineate completely the influence of temperature on the cocrystallization behaviour of these systems the phase diagrams are drawn in *Figures 3a-d*. In these phase diagrams the apparent melting points ( $T_m$ ) are plotted against the composition of blends crystallized at different temperatures. The equilibrium melting point ( $T_m^0$ ) of the cocrystals are also presented in these diagrams and will be discussed later. In *Figures 3a* and *b* the KF/KY and Cop-1/Cop-2 blends exhibit a linear dependency between the apparent melting points of the parent components with composition. However, in *Figures 3c* and *d* the melting point composition diagrams are of a different type than those of the former systems. In the KY/Cop-1 system (*Figure 3c*) cocrystals are not produced over the whole composition of the blend in any of the crystallization temperatures studied. There is a bifurcated area in the figure at each crystallization temperature and it represents the immiscibility in the solid state at these blend compositions. In *Figure 3d* similar but larger bifurcated areas have been observed indicating greater immiscibility of the KF/Cop-1 system than the KY/Cop-1 system. The reason for the larger immiscibility in the KF/Cop-1 system compared to that of the KY/Cop-1 system may be due to the larger difference in defect concentration in the former than that

in the latter pair. One interesting observation in this system is that the immiscibility area at first decreases with increase in crystallization temperature to 120°C and after that it again increases with increase in crystallization temperature to 135°C. The reason is yet uncertain and a probable cause for the decrease of the immiscibility area with increase in temperature may be due to the easier incorporation of H-H defect in the crystalline lamella at higher temperature producing cocrystal<sup>12</sup>. Support of this assertion comes from the fact that  $d_{hkl}$  of both the  $\alpha$  and  $\beta$  phases of PVF<sub>2</sub> increases with increase in  $T_c$  and this possibly occurs due to the incorporation of larger size H-H defect in the lamella<sup>18</sup> in greater numbers. The increase of immiscibility area at 135°C is due to the segregation of higher defect content fractions during crystallization from the melt as stated earlier.

#### Crystallization temperatures

The composition dependence of the crystallization temperatures ( $T_c$ s) of each blend has been presented in *Figure 4*. Single  $T_c$  offers secondary evidence of cocrystallization and have certain limitations as discussed below. In the figure KF/KY, Cop-1/Cop-2 and KY/Cop-1 systems exhibit linear plots of  $T_c$  with composition, whereas the KF/Cop-1 system shows bifurcation which suggests that they are not producing cocrystals at all compositions. It has been pointed out earlier that KF/KY and Cop-1/Cop-2 cocrystallize over the whole composition range. However, in the case of the KY/Cop-1 system there is some doubt. The exotherms of this system presented in *Figure 5*, are similar to those of the other cocrystal pairs. In *Figure 6* the melting



**Figure 3** (a) Phase diagrams of KF/KY PVF<sub>2</sub> blends crystallized at (a) 50°C, (b) 120°C, (c) 135°C and (d) equilibrium melting points. (b) Phase diagrams of Cop-1/Cop-2 blends crystallized at (a) 50°C, (b) 120°C and (c) equilibrium melting points. (c) Phase diagrams of KY/Cop-1 blends crystallized at (a) 50°C, (b) 120°C, (c) 135°C and (d) equilibrium melting points. (d) Phase diagrams of Kf/Cop-1 blends crystallized at (a) 50°C, (b) 120°C, (c) 135°C and (d) equilibrium melting points

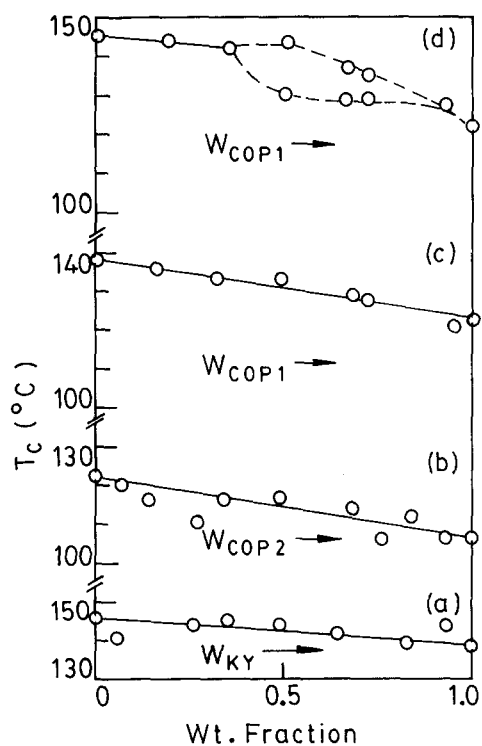


Figure 4  $T_c$  composition plots of (a) KF/KY, (b) Cop-1/Cop-2, (c) KY/Cop-1 and (d) KF/Cop-1 blends obtained from cooling the melt (227°C) at the rate of 2.5° min<sup>-1</sup>

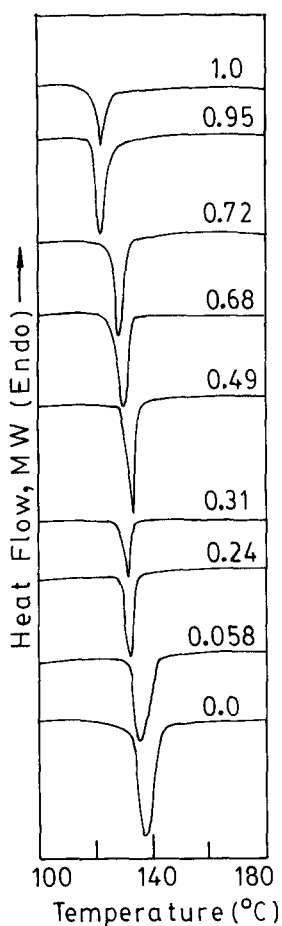


Figure 5 Crystallization exotherms of KY/Cop-1 blends obtained from cooling the melt (227°C) at the rate of 2.5° min<sup>-1</sup> for the indicated weight fraction of Cop-1

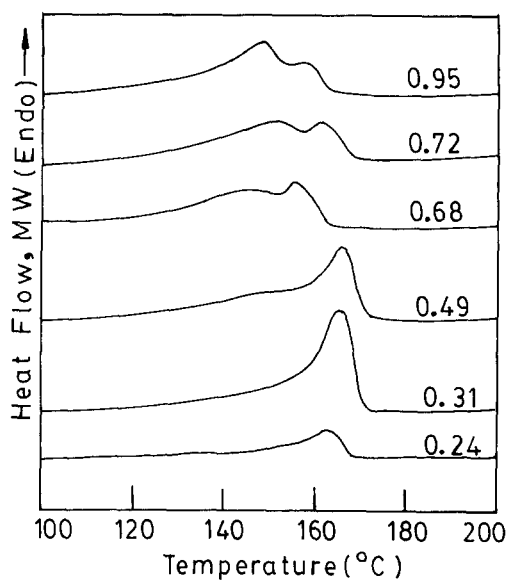


Figure 6 Melting endotherms of KY/Cop-1 blends crystallized as in Figure 5 at the indicated weight fraction of Cop-1

endotherms of KY/Cop-1 blends crystallized by the above procedure are presented. From the figure it is clear that for compositions  $W_{\text{Cop-1}} > 0.5$  the blends exhibit two peaks while for the composition  $W_{\text{Cop-1}} < 0.5$  they exhibit a single peak. Thus it may be concluded that KY/Cop-1 blends with  $W_{\text{Cop-1}} > 0.5$  are not producing cocrystals though they exhibit a single peak in the crystallization exotherms. The  $T_c$ s of the KY/PVF<sub>2</sub> and Cop-1 differ by 15° and is 8° less than that of the KF/Cop-1 system and it may be a cause to exhibit a single exotherm at Cop-1 rich blends of the KY/Cop-1 system. Thus the phase diagram based on crystallization temperature are less important compared to those based on melting temperature.

#### Equilibrium melting point

This section is much more important because it not only represents the characteristics of the crystalline state but it also reflects the thermodynamics of the liquid state in the melt. The equilibrium melting points were determined using Hoffman-Weeks procedure<sup>19</sup> taking the melting points as the same and low level of crystallinity (10%) of the blend at each crystallization temperature<sup>16,20</sup>. Here it is necessary to mention that equilibrium melting points of  $\alpha$  phase of PVF<sub>2</sub> and those of the  $\beta$  phase of copolymers were determined. The equilibrium melting points of the  $\gamma$  phase were not determined though it occurred in some PVF<sub>2</sub> blends.

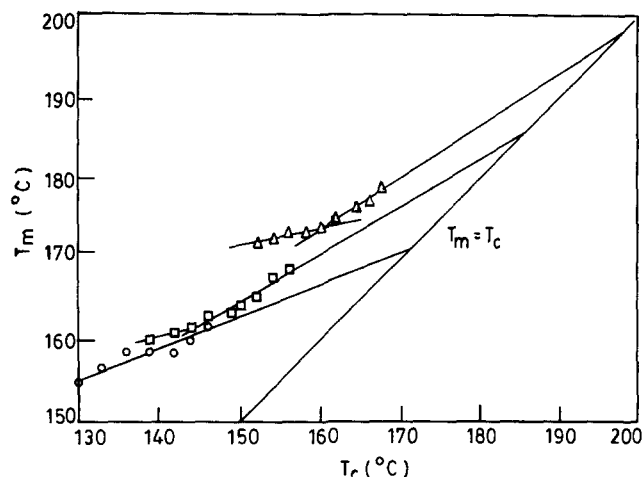
In Figure 7 the Hoffmann-Weeks plots of KF/KY, Cop-1/Cop-2 and KY/Cop-1 blends are shown for their 1/1 composition. As in the pure PVF<sub>2</sub> the plots of KF/KY and KY/Cop-1 systems show a break at lower crystallization temperature. The reason is the same as discussed earlier<sup>16,20</sup>. However, it may be pointed out that Cop-1, Cop-2 and their blends do not exhibit such a break in any of the composition. The equilibrium melting points and slopes of the upper portions of Hoffmann-Weeks plots are presented in Table 2. The slope values are close to the theoretical value of 0.5 and are similar to the values reported earlier<sup>16,20</sup>.

Some interesting thermograms of KY/Cop-1 blends at

**Table 2** Equilibrium melting points and slopes of Hoffman-Weeks plot of PVF<sub>2</sub> and VF<sub>2</sub>-VF<sub>4</sub> copolymer blends

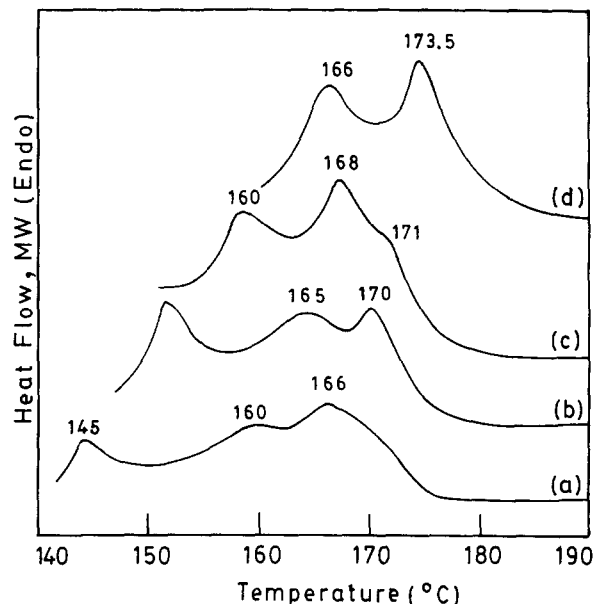
Blend	Composition <sup>a</sup>	Polymorph	Slope	T <sub>m</sub> <sup>0</sup> ± 2(°C)
KF/KY	0.0	α	0.72	213
	1.0	α	0.69	189
	0.25	α	0.71	202
	0.50	α	0.67	197.4
	0.75	α	0.58	186
Cop-1/Cop-2	0.0	β	0.44	173
	1.0	β	0.43	159
	0.25	β	0.46	172
	0.50	β	0.41	171
	0.75	β	0.38	162
KY/Cop-1	0.25	α	0.57	184
	0.50	α	0.59	185.6
	0.75	α	0.47	189
KF/Cop-1	0.25	α	0.68	210
	0.50	α	0.58	203
	0.75	α	0.71	213

<sup>a</sup>Weight fraction of higher H-H defect component of the blend



**Figure 7** Hoffman-Weeks plots at the 1/1 (by weight) composition of the blends.  $\Delta$ , KF/KY;  $\square$ , KY/Cop-1;  $\circ$ , Cop-1/Cop-2

composition  $W_{\text{Cop-1}} = 0.75$  during melting of isothermally crystallized samples are presented in Figure 8. For crystallization at 139°C two peaks (145°C and 166°C) and a hump (160°C) are observed and with increasing crystallization temperature the size of the hump increases to give the shape of a peak and clearly there are three peaks for crystallization at 145°C. With a further increase in  $T_c$  the highest temperature peak decreases in size and takes the shape of a hump at 152°C and at 158°C it vanishes showing only two peaks. The KF/Cop-1 system at composition  $W_{\text{Cop-1}} = 0.75$  also yields similar thermograms and the highest melting peak vanishes while crystallizing at 168°C. Both the KF and KY PVF<sub>2</sub> can crystallize in the  $\alpha$  and  $\gamma$  phases depending on the crystallization temperature, whereas Cop-1 crystallizes only in the  $\beta$  phase. If the components are miscible in the melt then crystallization in any of the  $\alpha$  or  $\beta$  polymorphs of PVF<sub>2</sub> takes place according to the resultant H-H defect concentration in the melt<sup>11,18</sup>. The  $\gamma$  polymorph is usually produced at higher temperature

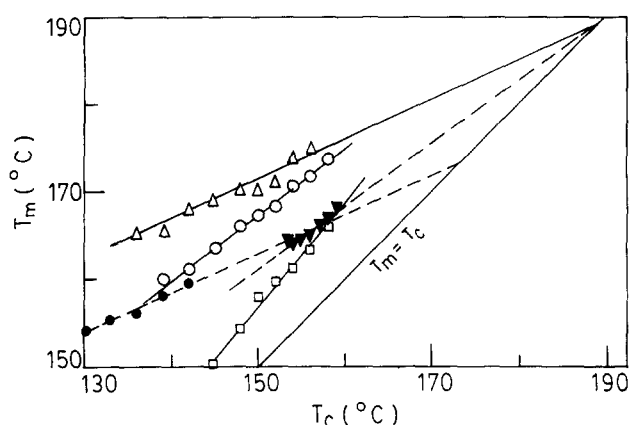


**Figure 8** Melting endotherms of isothermally crystallized KY/Cop-1 blend ( $W_{\text{Cop-1}} = 0.75$ ) (10% crystallinity) crystallized at different crystallization temperatures (a) 139°C, (b) 145°C, (c) 152°C and (d) 158°C. The d.s.c. was scanned from the  $T_c$  at 10° min<sup>-1</sup> without cooling

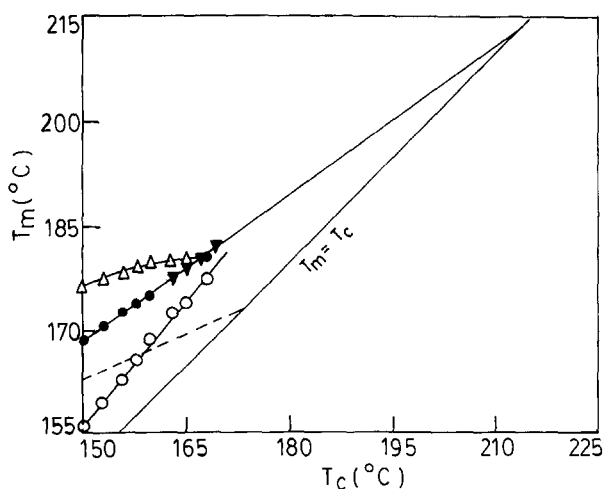
and it increases with increase in crystallization temperature<sup>21</sup>. The highest temperature peak is not, therefore, due to the  $\gamma$  phase because the peak area decreases with increase in  $T_c$ . To find the origin of the three peaks we made  $T_m-T_c$  plots which are shown in Figure 9, where the  $T_m-T_c$  plots of pure KY and Cop-1 are also presented. From the figure it is apparent that the  $T_m-T_c$  line of the lowest melting peak is lower than those of Cop-1 and KY PVF<sub>2</sub>, while the  $T_m-T_c$  lines of the other two melting peaks are higher than those of Cop-1 and KY PVF<sub>2</sub>.

To explain this phenomenon it may be argued that there is structural heterogeneity in both the KY PVF<sub>2</sub><sup>16</sup> and Cop-1 and the highest regular fraction of KY PVF<sub>2</sub> produces the highest melting peak, the lowest regular fraction of Cop-1 produces the lowest melting peak and

the lower regular fraction of KY and the higher regular fraction of Cop-1 produces the middle melting peak. The apparent melting points conform to such a fractionation process. But how does such a fractionation occur? It is possible in two ways: (a) liquid-liquid phase separation; and (b) liquid-crystal phase separation. The latter possibility can be ignored because the highest melting peak gradually decreases with increasing  $T_c$  and vanishes when crystallized at 158°C. If it is fractionation due to crystallization the highest temperature peak should be sharper with increasing  $T_c$  because fractionation is favoured at higher  $T_c$ . Therefore, the fractionation is occurring due to the liquid-liquid phase separation<sup>22</sup> and here it is a three phase system. Although in the ternary systems two phase regions are more common<sup>24</sup>, three phase regions are also possible as suggested by Tompa<sup>24,25</sup>. Koningsveld *et al.* observed three phases in binary polymer solvent systems with broader molar mass distribution of the polymer<sup>26,27</sup> and three liquid phases also occurred in the binary blends of linear polyethylene with branched polyethylene<sup>28</sup>. Thus, in the binary system with wider structural heterogeneity, three liquid phases are possible and we can propose that in the binary blends



**Figure 9** Hoffman-Weeks plots of KY/Cop-1 blend ( $W_{\text{Cop-1}} = 0.75$ ): □, for the lower melting peak; ○, for the middle melting peak; △, for the higher melting peak; ●, for Cop-1; and ▼, for KY<sup>16</sup>



**Figure 10** Hoffman-Weeks plots of KF/Cop-1 blend ( $W_{\text{Cop-1}} = 0.75$ ): ○, for the lower melting peak; ●, for the middle peak; △, for the higher melting peak; ▼, data of pure KF<sup>16</sup>; the dotted line indicates the  $T_m - T_c$  line of Cop-1

of PVF<sub>2</sub> and VF<sub>2</sub>-TFE copolymer three liquid phases produce three crystalline phases which show the three melting peaks during melting. In *Figures 9 and 10* the Hoffman-Weeks plots to obtain  $T_m^0$  of the ternary systems have been shown. There is some difference in two plots. *Figure 9* shows that the lower and middle melting peak cannot be extrapolated to the  $T_m = T_c$  line, but the higher melting temperature can be extrapolated to yield  $T_m^0$  value. In the KF/Cop-1 system (*Figure 10*) the situation is different and here the middle peak can be extrapolated to yield a  $T_m^0$  value equal to that of KF but not the others. The cause of difference in extrapolation of the melting peaks of KF/Cop-1 and KY/Cop-1 blends ( $W_{\text{Cop-1}} = 0.75$ ) to  $T_m = T_c$  line is not known. A probable reason may be due to the difference in the ternary phase diagrams and also due to the difference in their temperature variation of the last two systems<sup>28</sup>. The same  $T_m^0$  values of the blends to those of pure KF and KY PVF<sub>2</sub> suggest that there is no favourable interaction at this composition of KF/Cop-1 and KY/Cop-1 blends required for mixing<sup>20</sup>.

Now we want to discuss the  $T_m^0$ -composition plots of the systems (*Figures 3a-d*). The KF/KY blends have a concave upward curve and this indicates that there is weak attraction between the components of the system<sup>8</sup>. However, Cop-1 + Cop-2 blends exhibit a linear plot joining those of the components indicating that mixing is ideal. But with increasing difference in defect concentration of the components the nature of the plot is different having both concave upward and concave downward portions. By analogy to the Gibbs free energy of mixing of binary mixtures<sup>24</sup> we can predict that the concave downward portion is metastable and is liable to phase separation both in the melt as well as in the crystalline state. These  $T_m^0$ -composition plots also indicate that the interaction parameter is composition dependent in both the KF/Cop-1 and KY/Cop-1 system and this fulfils the requirement for the formation of a three phase system<sup>27</sup> in the Cop-1 rich regions of KF/Cop-1 and KY/Cop-1 blends. The liquid-liquid phase separation in the melt, therefore, hinders the cocrystallization at  $W_{\text{Cop-1}} \sim 0.6-0.9$  for KY/Cop-1 blends and at  $W_{\text{Cop-1}} \sim 0.7-0.95$  for KF/Cop-1 blends.

## CONCLUSION

Cocrystallization of PVF<sub>2</sub> is very much dependent on the H-H defect present in the parent components and if the difference is low it can co-crystallize in all the compositions at all the temperatures. But if the difference is large cocrystallization is dependent on the crystallization temperature and also on the composition of the blends. The cocrystallization in some cases is hindered due to the fractionation of higher defect content material during crystallization at high temperature. The crystallization temperature composition data cannot yield a true phase diagram of the system. The cause for not forming a cocrystal of KF/Cop-1 and KY/Cop-1 blends at Cop-1 rich regions is expected due to the liquid-liquid phase separation of the system, and where both binary and ternary phase may be possible. Thus the cocrystallization of PVF<sub>2</sub> and VF<sub>2</sub>-VF<sub>4</sub> copolymers is a complex process and it is hindered by both liquid-liquid and liquid-crystal phase segregation processes depending on blend composition and crystallization temperature.



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